

10/534642

[10191/3848]

7/PRts.

METHOD AND DEVICE FOR ADAPTIVELY CONTROLLING POWER

Field of the Invention

5 The present invention is directed to a method and a device for adaptively controlling power of transmitted signals of a radar detector.

Background Information

10 In the automotive sector, systems which measure the distances and velocities of objects around one's own vehicle by using microwaves and applying the radar principle are in use. These objects can be vehicles which are actively taking part in the highway traffic or some sort of obstacles on or near the road. Keyless remote-entry systems for vehicles (keyless entry/comfort entry/keyless go systems) also make use of these

15 technologies. In the known systems, high-frequency energy is radiated in a frequency range in the gigahertz range, at a mid-frequency of 24,125 GHz and with a two-way bandwidth of several GHz. Typical antennas have a directional characteristic (i.e., an antenna radiation pattern) of 80

20 degrees * 20 degrees. In practice, the transmission range is about 20 m. The risk inherent in such systems is that unacceptably high signal levels occur, even in frequency ranges that have been blocked in favor of other services, e.g., frequency ranges that are reserved for radio astronomy

25 or also for radio relay services. Unacceptably high signal levels can occur, for example, when a substantial number of the above-mentioned systems in the surrounding, for example several hundred, are simultaneously put into operation. This

can be the case, for example, when a large number of vehicles are moving on multilane urban streets. Similar problems arise in large parking lots at sports facilities or shopping centers when, for example, after a big event ends, hundreds of

5 vehicles start moving at the same time and leave the parking lot. For the most part, these problems only occur when the vehicles are at standstill or traveling at a relatively slow speed. This is because, at higher speeds, the distances between the vehicles increase again, and the vehicle density
10 decreases correspondingly. Furthermore, the spatial proximity of many sensors also causes heavy mutual interference, which, when working with adaptive sensors, increasingly leads to additional measurements being taken, although some objects may have actually already been reliably detected.

15 Published German Patent Application DE 100 65 521 describes a method and a device for detecting moving or stationary objects using radar radiation, in particular for use in motor vehicles, where, in order to detect objects, pulse-modulated carrier waves are radiated, whose reflected portions are then
20 received and evaluated. In this context, by transmitting an unmodulated carrier in the time intervals between two adjacent pulses, a Doppler measurement can additionally be performed, thereby enabling a reliable velocity measurement to be taken.

When irregularities are detected in received signals, the
25 transmitting branch of the radar may be switched off. Thus, no more transmission signals are emitted by the transmitting antenna. However, correlation pulses from a pulse transmitter continue to be transmitted to the receiving branch of the radar sensor. If it turns out in the process that object
30 information is still received, then an illusory object must be inferred.

Summary

The present invention minimizes signal irregularities in radar detectors by using an adaptive power control. As soon as it becomes apparent that the interference is unacceptably high
5 due to a heavy traffic density, an appropriate power adaptation is carried out. Once objects have been reliably detected, the measurement repetition rate may be reduced. In addition, the possible detection range does not need to be utilized up to the maximum value; instead, it may be stopped
10 once a limit to be regarded as useful is reached, such as of two to five detected objects, especially as the power requirement increases with the fourth power of the distance. Provided that a ground speed is measurable, at a low speed of less than about 20 to 40 km/h or at standstill, and in the
15 case of far away objects, the power may likewise be reduced by limiting the average power, the measurement repetition frequency, or the maximum distance. The relatively low speed makes it unlikely that objects would appear unexpectedly. If necessary, however, a measurement may also be made in-between,
20 up to the maximum range, in order to secure the intervening space up to the furthest object, and thereby enhance the safety on the whole. The speed information may be obtained from the wheel speeds, from a radar measurement which records the ground speed, or from an SRR (secondary surveillance
25 radar) measurement by estimating stationary objects. While the first two mentioned methods lead to very reliable results, the last-mentioned method additionally requires an exact classification into illusory objects, on the one hand, and tangible moving objects, on the other hand, to attain reliable
30 results. Since in situations of high traffic density and, thus, a high concentration of sensors, the interfering influences increase, in which case the present invention also

makes it possible to adaptively reduce the power within a relatively short range, provided that reliably detected objects exist. The present invention makes it possible for the transmitting power to be reduced, thereby facilitating an approval in conformance with UWB (ultra-wide band) criteria. By reducing the transmitting power, the interference immunity may be further enhanced. This means that there is less mutual interference among adjacent vehicles. The reduced transmitting power leads to a lower current consumption, which is beneficial in terms of energy usage. Also, because of the reduction in load, one can expect a longer service life. By applying the approach of the present invention, assuming a maximum distance of 20 m and a breaking off of the emissions in the distance stages 5m, 10m or 15 m, the average power could be reduced by 30 db, 15 db, and 6 dB, respectively. Consequently, the spectral density is, of course, also lowered. In addition, the transmitted power could also be lowered by approximately 6 to 20 dB.

Brief Description of the Drawings

Figure 1 shows a conventional radar device of the related art;

Figure 2 shows a motor vehicle having radar devices.

Figure 3 shows a graph of a radar signal of a radar device.

Figure 4 shows a graph of radar signals having interference of varying intensity.

Figure 5 shows a block diagram of a radar device.

Figure 6 shows a first flow chart illustrating the reduction of power.

Figure 7 shows a second flow chart illustrating the reduction of power.

Detailed Description

In a block diagram, Figure 1 shows a radar device having a correlation receiver as known in the art. A pulse generator 2 induces a transmitting device 1 to emit a transmitted signal 6 via an antenna 4. Transmitted signal 6 impinges on a target object 8, where it is at least partially reflected, and returns to receiver 14. Received signal 10 is received by antenna 12. In this context, antenna 12 and antenna 4 may be identical and be switched between transmitting and receiving operation. Upon receipt of received signal 10 by antenna 12, received signal 10 is routed to receiver 14 and subsequently fed via a filter device having A/D conversion 16 to an evaluation device 18. An exceptional feature of such a radar device, which has a correlation receiver, is that receiver 14 receives a reference signal 20 from pulse generator 2. Received signals 10 received by receiver 14 are mixed in receiver 14 with reference signal 20. The correlation operation makes it possible to infer the distance of a target object, for example, on the basis of the temporal delay from emission of a radar signal until receipt of a radar signal reflected off of a target object.

It is possible to operate a plurality of substantially identical, e.g., between 4 and 16, radar sensors on one vehicle. This is clearly shown in Figure 2, which illustrates a motor vehicle 20 having a multiplicity of radar sensors 21. Radar sensors 21 are interconnected via a bus to one another and to control devices. For example, a device 24 for providing a park distance control and for detecting a blind spot, a device 26 for the precrash function, as well as a

device 28 for facilitating travel in stop-and-go traffic are provided.

Figure 3 shows a typical radar signal which is transmitted by a radar device working in the short range. When working with a radar device of this kind, high-frequency energy is radiated in a frequency range in the gigahertz range, at a mid-frequency of 24,125 GHz and with a two-way bandwidth of several GHz.

Figure 4 shows typical received signals which have been picked up by a radar device working in the short range. The characteristic curve of first received signal ES1 shown in the upper part of the diagram is substantially undisturbed. The characteristic curve of second received signal ES2 shown in the middle area of the diagram is influenced by a strong interference, which may be caused by an FMCW (frequency modulated continuous wave) radar. Third received signal ES3 illustrated in the lower part of the diagram is affected by a very strong interference of the same type.

Figure 5 shows a block diagram of a radar device 520 which is provided for monitoring the immediately adjacent zone around a motor vehicle. A control device 522 supplies energy to radar device 520. Thus, for example, control device 522 supplies an input voltage of 8 V for radar device 520. This input voltage is fed to a DC/DC converter 524 which makes available a supply voltage of, for example, 5 V for the components of radar device 520. Radar device 520 also includes a local oscillator 526 which produces a carrier frequency of 24 GHz, for example. This local oscillator is supplied with a bias voltage generated by a converter 530, which is driven by pulses produced by a clock-pulse generator 528. The pulses produced by clock-pulse generator 528, which may have a frequency of a

few MHz, e.g., 5 MHz, are used to modulate the carrier signal supplied by local oscillator 526. This modulation is carried out in the transmitting branch of radar device 520 by a switching element 532 which is controlled by a pulse shaper 546. Pulse shaper 546, in turn, is likewise driven by the clock frequency of clock-pulse generator 528. The pulsed signals generated in this manner are radiated by an antenna 534. In the case that the signals emitted by antenna 534 are reflected off of a target object, for example, the reflected signals are received by an antenna 536. Once the received signals are amplified in an amplifier 538, the signals are fed to two mixers 540 and 542. First mixer 540 then emits a so-called I-signal, while second mixer 542 outputs a 90° out-of-phase Q-signal. In mixers 540, 542, the received signals are mixed with the pulsed signals of local oscillator 526, this pulsing taking place via a switch 544. Switch 544 is driven by a pulse generator 548 which outputs delayed pulses. For example, pulses output by pulse generator 548 are delayed by a time period Δt with respect to the pulses from pulse generator 546. This delay is effected by a delay circuit 500. The duration of the delay of delay circuit 500 is influenced via a microcontroller 552, which preferably includes a digital signal processor. This is accomplished via a first analog output 554 of microcontroller 552. Via a second analog output 560, the I- or Q-signals processed by an amplifier 556 are influenced by another, e.g., variable amplification in amplifier 558. This amplifier 558 is controlled by a second analog output 560 of microcontroller 552. The output signal from amplifier 558 is fed to an analog input 562 of microcontroller 552. Microcontroller 552 communicates via an input/output bus 564 with control device 522. Radar device 520 also includes a so-called notch filter 566, which is suited for suppressing monochromatic or nearly monochromatic

interference signals. Also provided are a PLL (phase-locked loop) circuit 568 and a further mixer 570. The frequency of an interference signal may be advantageously determined by tuning PLL circuit 568.

5 Using the above-described device, it is possible to ascertain interference in the received signal and to classify the type of interference. At this point, as soon as it is determined that the detected interference is attributable to a high traffic density, an appropriate power adaptation, which may
10 contribute to a reduction in the interference, is carried out in accordance with the present invention. Once objects have been reliably detected, the measurement repetition rate may also be reduced. Since fewer radar signals are emitted as a result, the probability of interference being caused is also
15 reduced. In addition, it is not necessary to utilize the maximum possible detection range; instead, the detection range may be stopped once a limit to be regarded as useful is reached, e.g., two to five detected objects, especially as the power requirement increases with the fourth power of the
20 distance. This is explained below with reference to the flow chart of Figure 6.

In a first step 60, radar device 520 is operated in normal operation. In this normal operation, measurements are taken at regular intervals up to a maximum range of about 20 m. In a
25 step 61; it is checked whether objects have been detected within a relatively short range. If this is not the case, alternative path 61a is selected, and the normal operation is continued in accordance with step 60. If, on the other hand, objects are detected within the relatively short range,
30 alternative path 61b is selected, and power is reduced in accordance with step 62 in that measurements are still only taken up to a limiting distance of n m, where $n < 20$ m. By

applying the approach of the present invention, assuming a maximum distance of 20 m and limiting the emissions at the distance stages 5m, 10m or 15 m, the average power could be reduced by 30 db, 15 db, and 6 dB, respectively. Consequently, the spectral density is, of course, also lowered. In addition, the transmitted power could also be lowered by approximately 6 to 20 dB.

An alternative approach for reducing power is explained with reference to the flow chart shown in Figure 7. In a first step 70, radar device 520 is operated in normal operation. In this normal operation, measurements are taken at regular intervals up to a maximum range of about 20 m. In a subsequent step 71, it is checked whether the vehicle is stationary or whether it is moving at a relatively low speed. If this is not the case, alternative path 71b is selected, and the normal operation is continued in accordance with step 70. If, however, only a low speed of less than about 20 to 40 km/h is measured, or it is determined that the vehicle is stationary, alternative path 71a may be taken to arrive at step 72. In this step 72, it is checked whether objects have been detected in a distance shorter than 20 m. If this is the case, alternative path 72a is selected, and power is reduced in accordance with step 73 in that measurements are still only taken up to a limiting distance of n m, where $n < 20$ m. The relatively low speed makes it unlikely that objects would appear unexpectedly. If necessary, however, a measurement may also be made in-between, up to the maximum range, in order to secure the intervening space and thereby enhance the safety on the whole. If this is not the case, alternative path 72b is selected, and the normal operation is continued in accordance with step 70.

The speed information may be obtained from the wheel speeds, from a radar measurement which records the ground speed, or

from an SRR (secondary surveillance radar) measurement by
estimating stationary objects. While the first two mentioned
methods lead to very reliable results, the last-mentioned
method additionally requires an exact classification into
5 illusory objects, on the one hand, and tangible moving
objects, on the other hand, to attain reliable results. Since
in situations of high traffic density and, thus, a high
concentration of sensors, the interfering influences increase,
the present invention also makes it possible to adaptively
10 reduce the power within a relatively short range, provided
that reliably detected objects exist. The present invention
makes it possible for the transmitting power to be reduced,
thereby facilitating an approval in conformance with UWB
(ultra-wide band) criteria. By reducing the transmitting
15 power, the interference immunity may be further enhanced. This
means that there is less mutual interference among adjacent
vehicles. The reduced transmitting power leads to a lower
current consumption, which is beneficial in terms of energy
usage. A longer service life may be expected as well, due to
20 the reduction in load.